

# **Performance of Continuous PM<sub>2.5</sub> Monitors at a Monitoring Site in Ottawa, Canada**

**Tom Dann**

**Luc White, Alain Biron**

**Environment Canada, ETC, Ottawa**

NESCAUM Monitoring and Assessment Committee Meeting  
May 7 & 8, 2008



**Environment  
Canada**

**Environnement  
Canada**

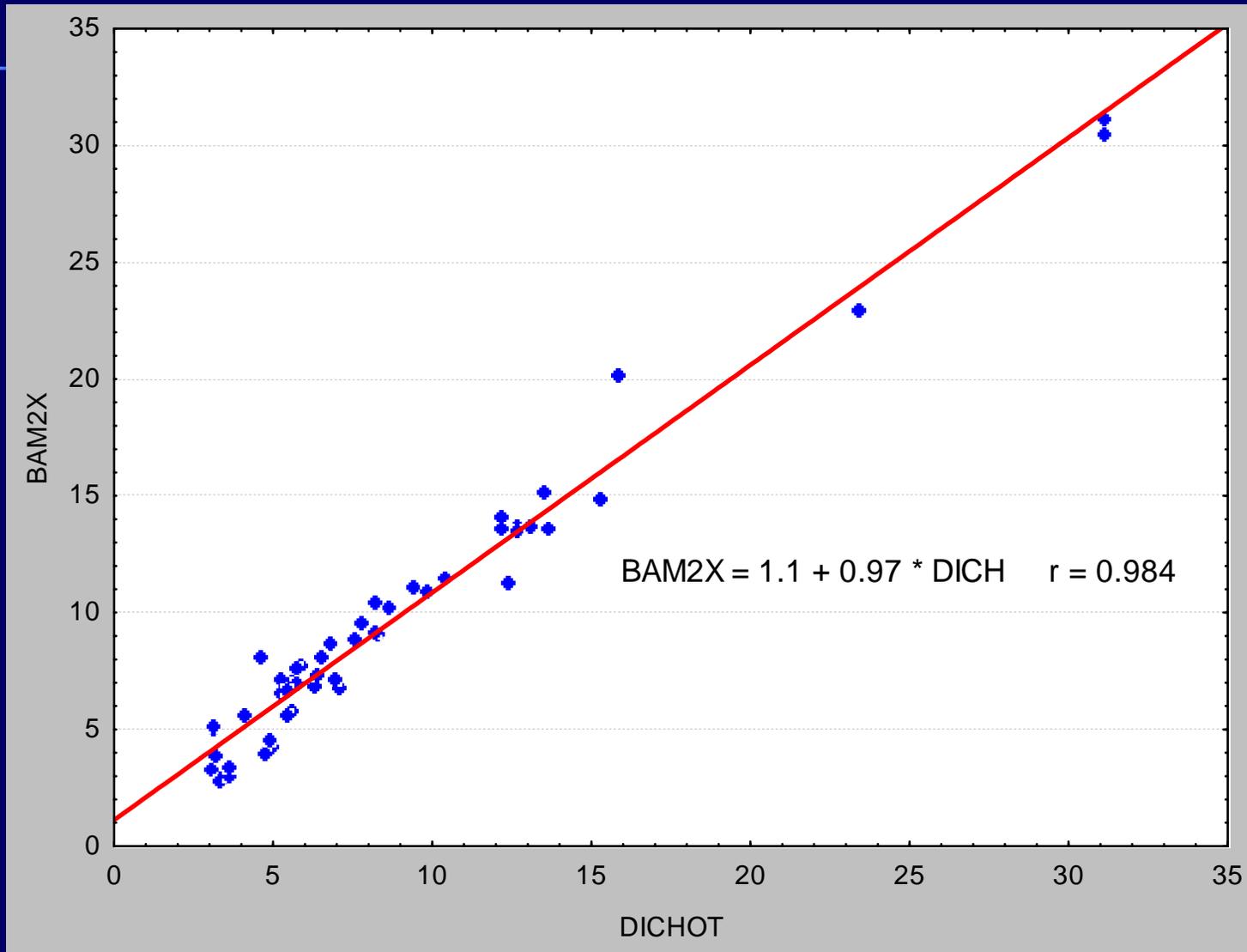
## Ottawa Monitoring Site

- Met-One BAM 1020 May 2004
- Met-One BAM 1020 (new) Nov 2006
- Met-One BAM 1020(2x) July 2007
- TEOM SES (30°C) May 2004
- TEOM FDMS July 2004
- GRIMM 180 (PM<sub>10</sub>, PM<sub>2.5</sub>, PM<sub>1.0</sub>) Oct. 2005
- Thermo SHARP 5030 June 2006

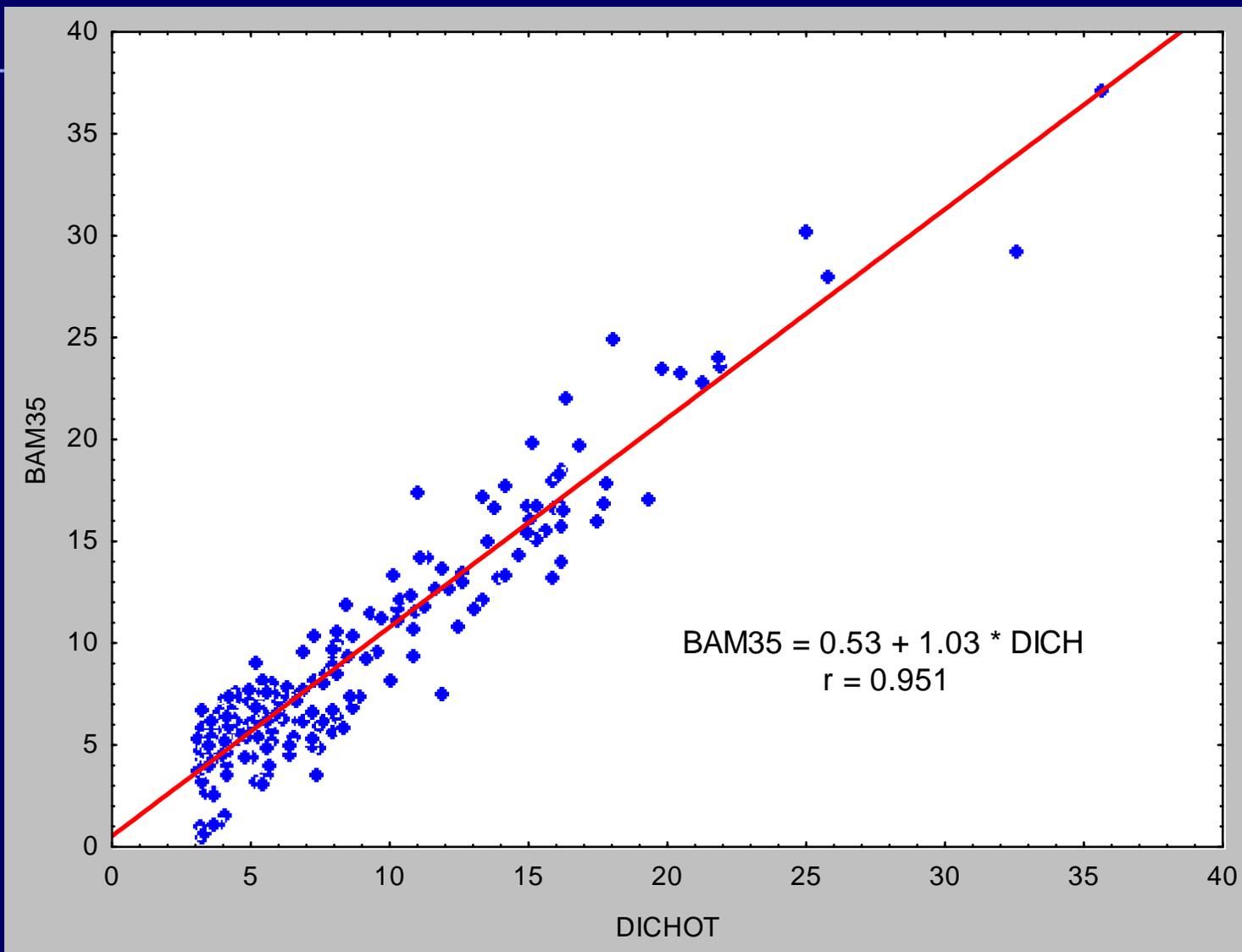
# Met-One BAM 1020(2x)

- first continuous PM<sub>2.5</sub> instrument to receive EPA Class III Equivalency designation
- designation achieved with a 35% RH setting on smart heater
- improved detection level and precision due to redesigned tape transport system
- close geometry beta source configuration
- count time 8 minutes and sample time 42 minutes
- firmware revision 3.2.4
- VSCC (not in Ottawa)
- outside pressure sensor and reporting at actual conditions (not in Ottawa)

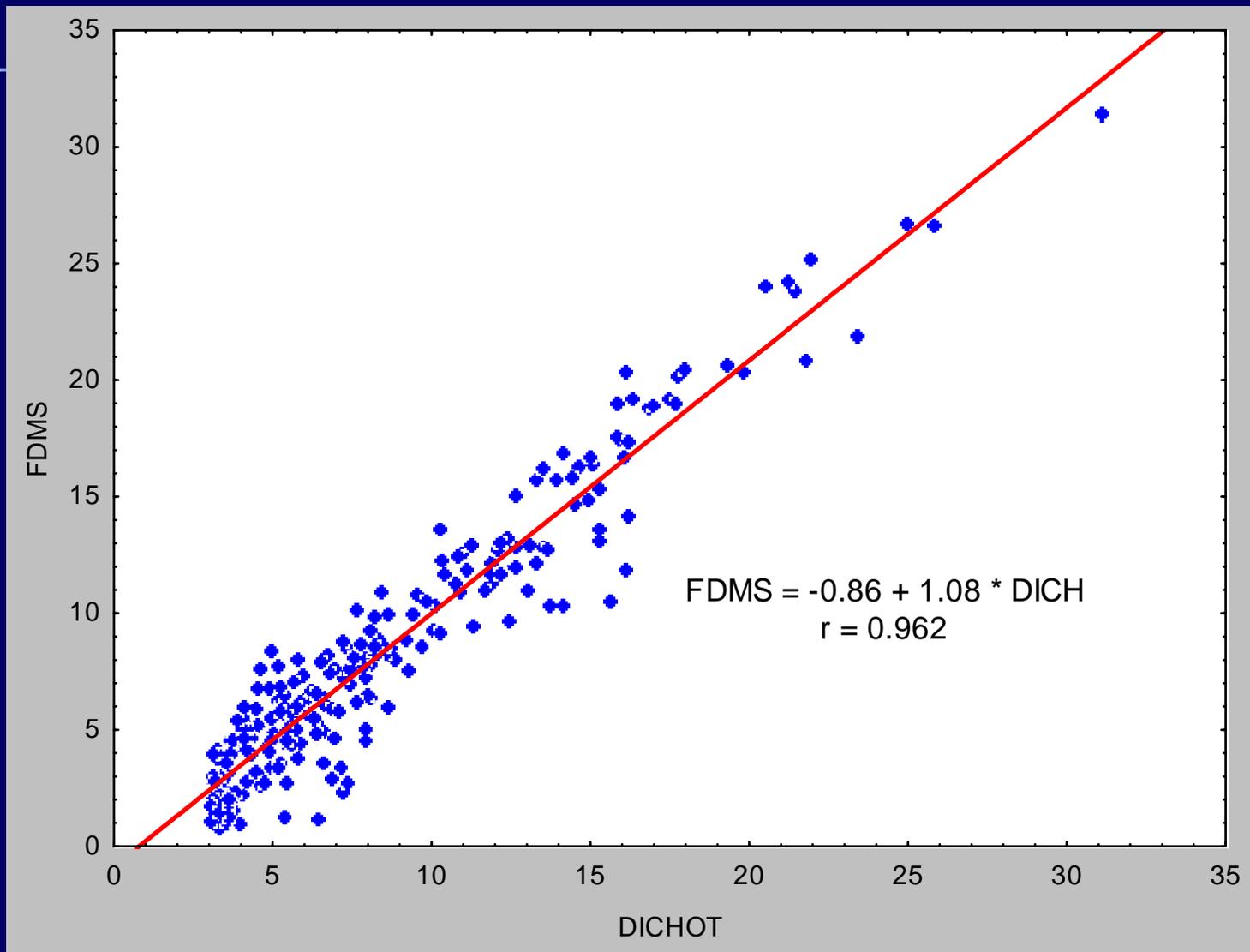
# Linear regression results for 24h data BAM 2x Ottawa (2007 - 2008)



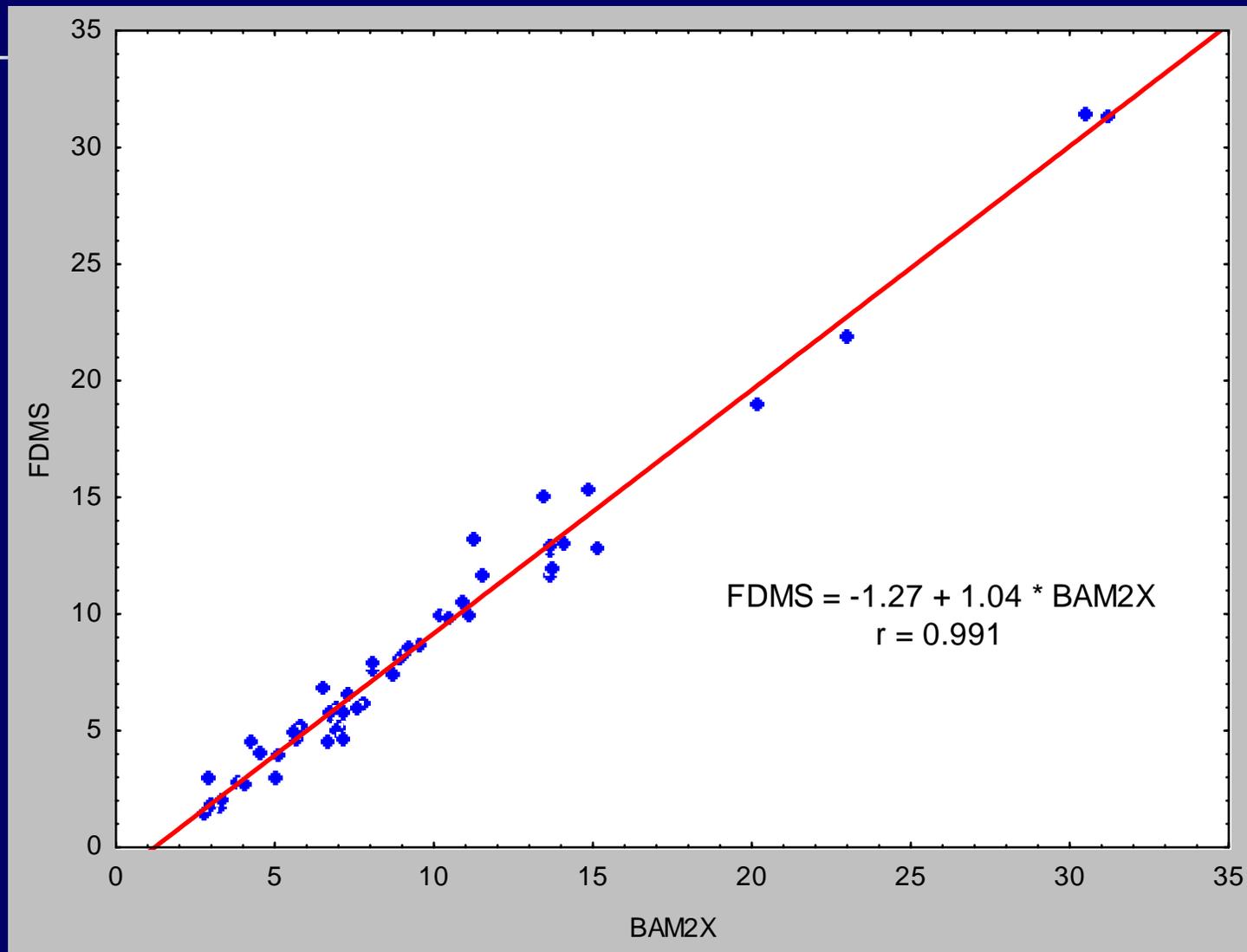
# Linear regression results for 24h data BAM 1020 Ottawa (Nov 2006 - Jan 2008)



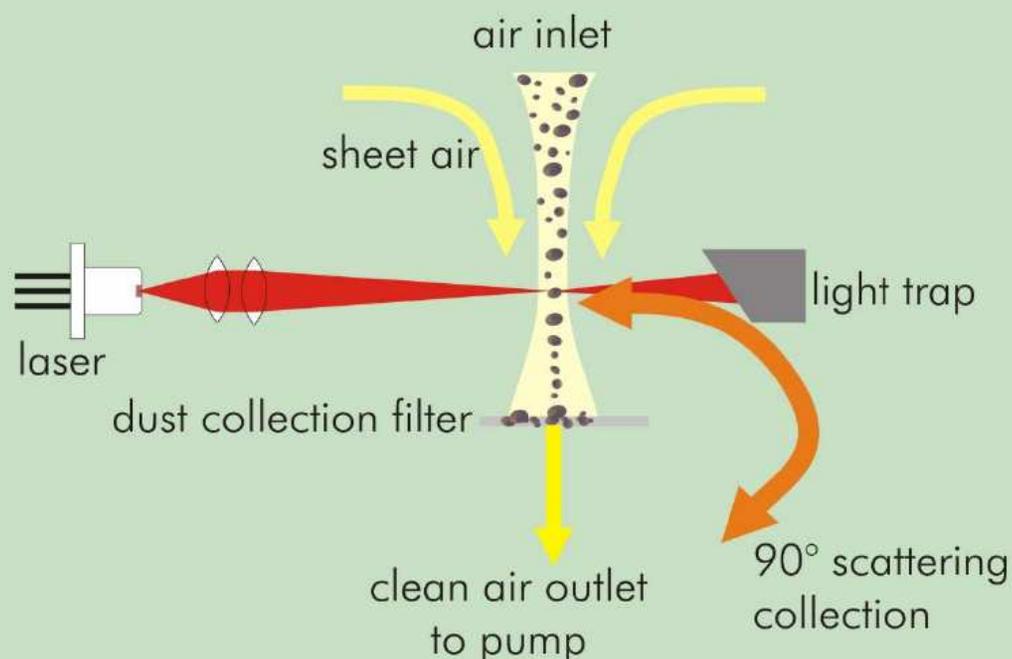
# Linear regression results for 24h data TEOM-FDMS Ottawa (2006-2008 All Data)



# TEOM-FDMS vs. BAM1020(2x) Ottawa (2007 - 2008 All Data)

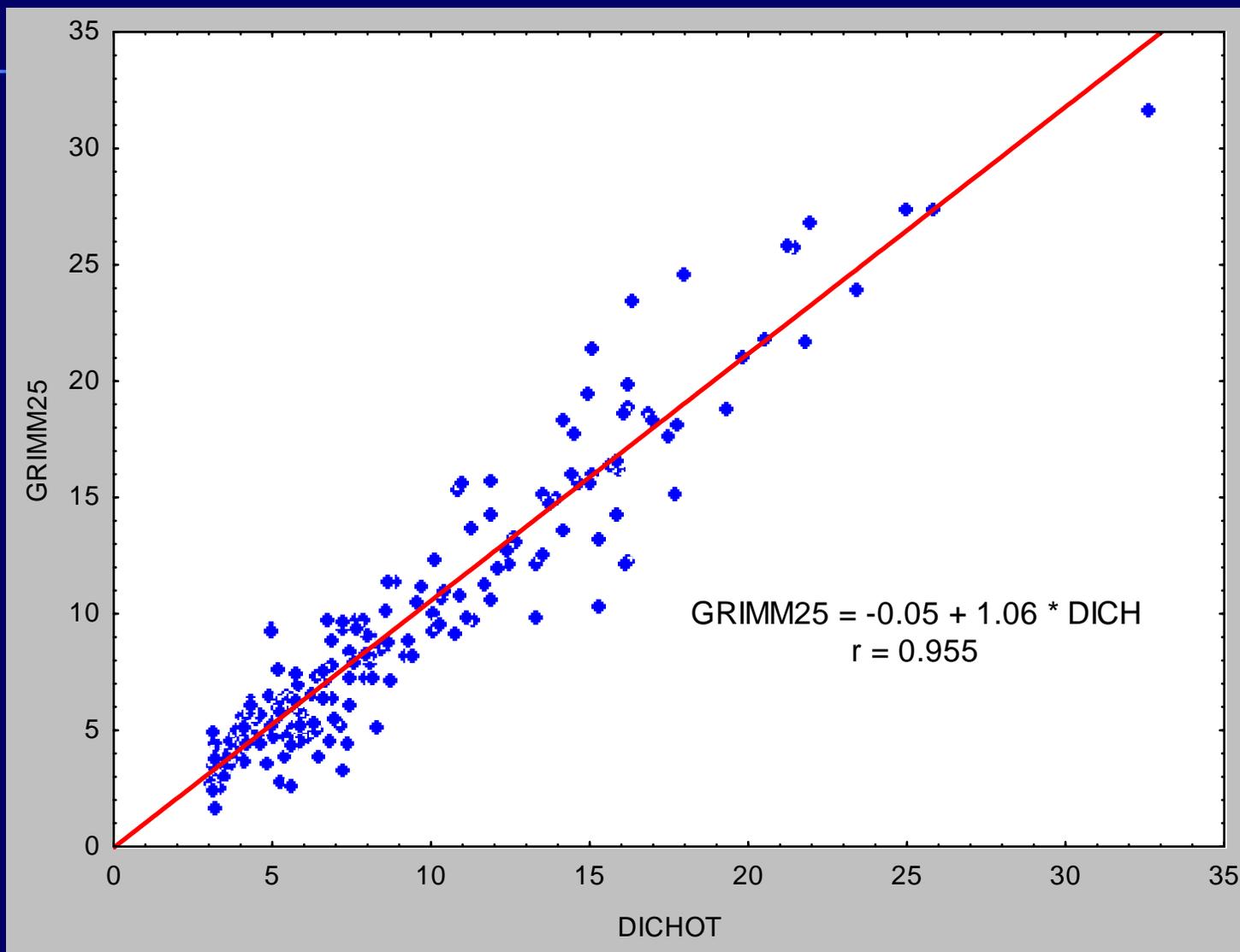


# Grimm 180 Multi-channel Aerosol Spectrometer

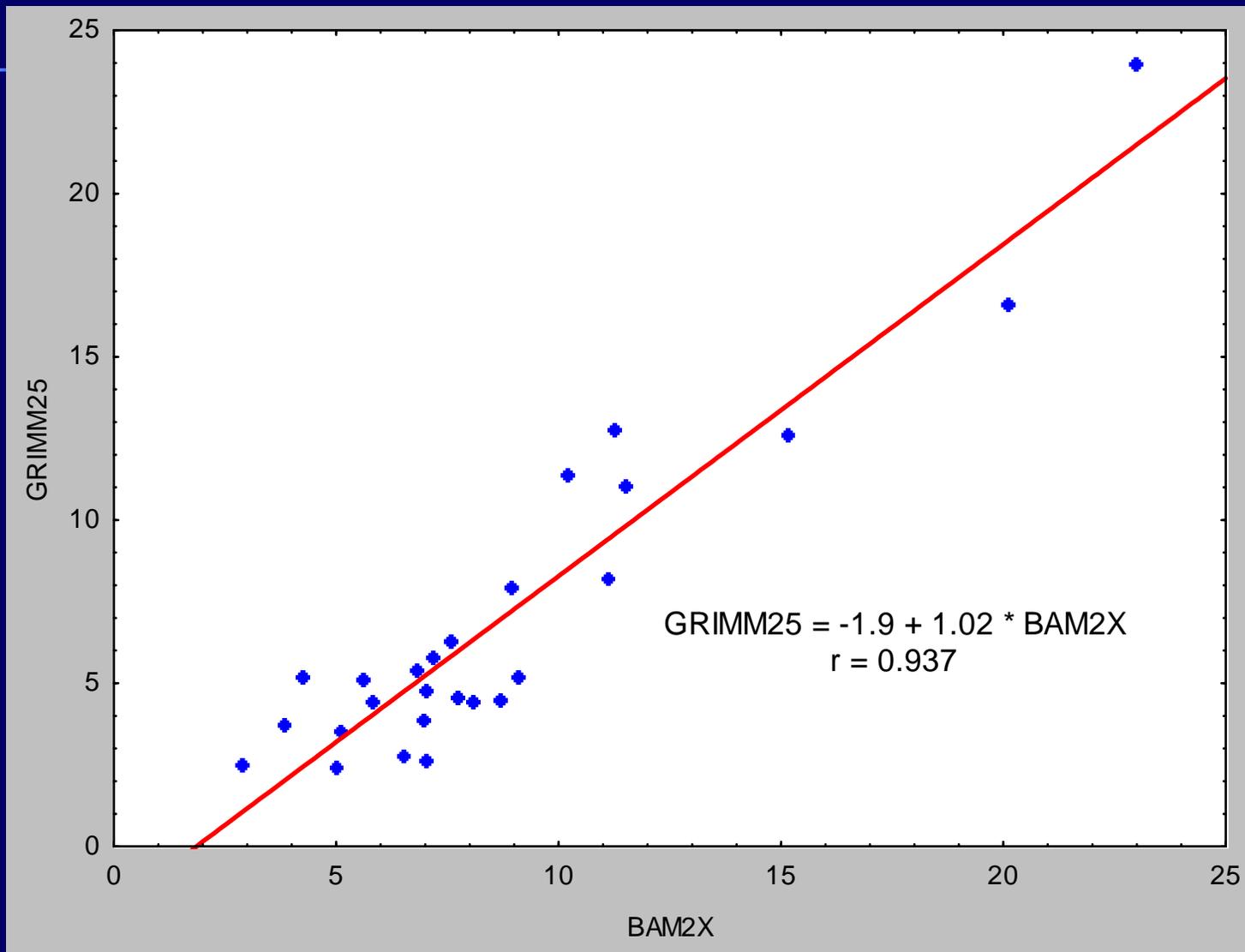


**Simultaneous measurement of PM<sub>1.0</sub>, PM<sub>2.5</sub> and PM<sub>10</sub>**  
**Particle counts by size (31 channels) and mass determination using algorithms**  
**No size cut on inlet – moisture control using Nafion dryer**  
**Truly continuous (real-time)**

## Results for 24h PM<sub>2.5</sub> data: Grimm 180 (Ottawa) Jan. 2006 – Dec. 2007



# Grimm 180 vs. BAM1020(2x) (Ottawa) July 2006 – Dec. 2007



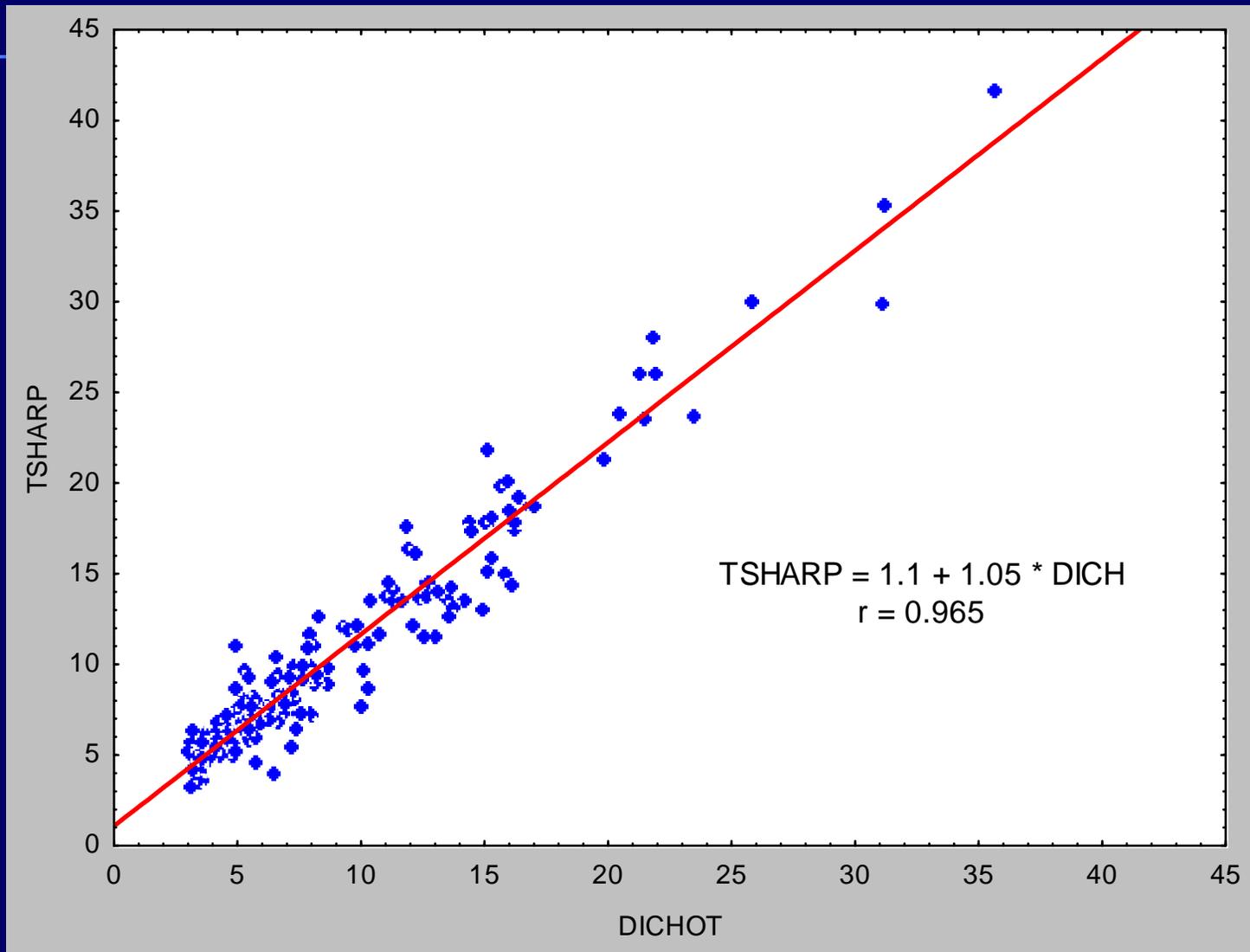
# Thermo SHARP 5030

## Synchronized Hybrid Ambient Real-time Particulate Monitor

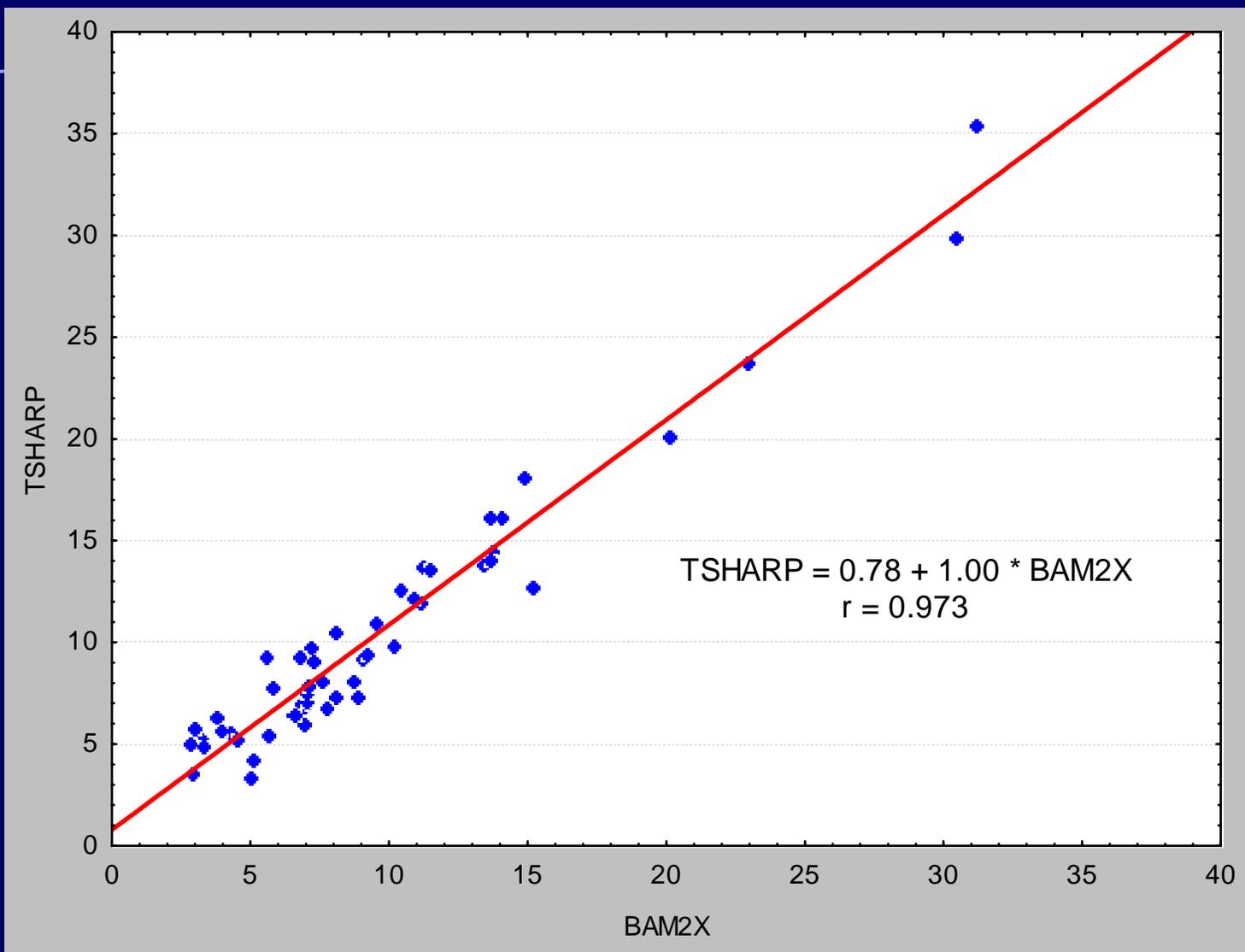


- Truly continuous (real-time)
- Combination nephelometer & beta-ray attenuation
- Light scattering photometer is continuously calibrated by beta attenuation mass sensor
- Intelligent Moisture Reduction (IMR) System heating the inlet tube; threshold is set at 40%

## Linear regression results for 24h data: Sharp 5030 (Ottawa June 2006 – Jan. 2008)



# Sharp 5030 vs. BAM1020(2x) (Ottawa July 2007 – Jan. 2008)



## Cost Comparisons for Continuous PM<sub>2.5</sub> Instruments (2007 Canadian\$):

- |   |          |
|---|----------|
| ▪ Met-One BAM 1020  | \$23,300 |
| ▪ Thermo TEOM 1405  | \$22,000 |
| ▪ Thermo 8500 FDMS Kit  | \$10,700 |
| ▪ TEOM-FDMS 1405-F  | \$31,300 |
| ▪ GRIMM 180 (PM <sub>10</sub> , PM <sub>2.5</sub> , PM <sub>1.0</sub> ) | \$34,000 |
| ▪ Thermo SHARP 5030   | \$26,500 |

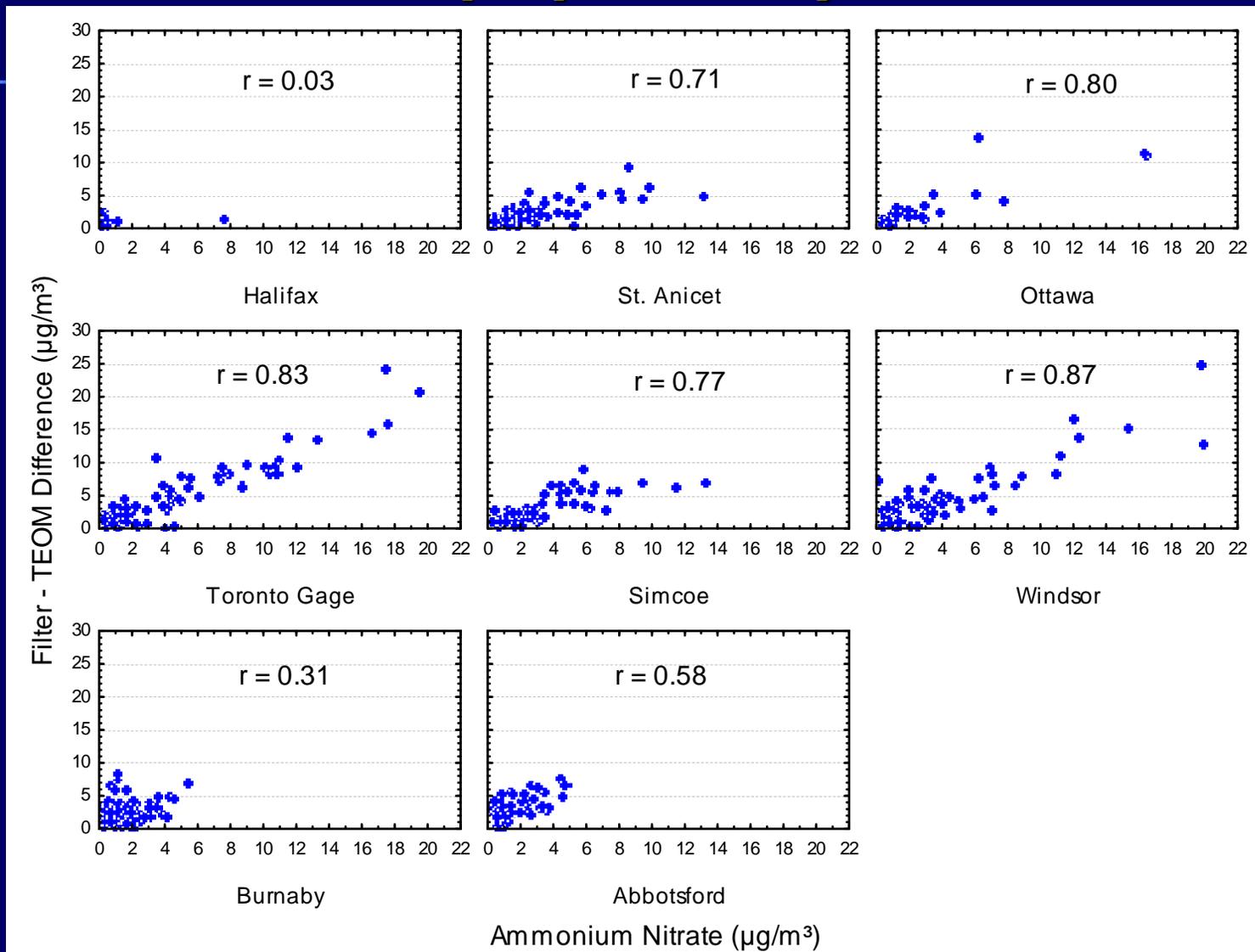
## 2007 Instrument Performance in Ottawa Based on EPA ARM Template

Instrument	N	Slope	Intercept	r
TEOM-SES	133	0.80	0.04	0.940
TEOM-FDMS	98	1.06	-0.96	0.966
BAM1020(2x)	52	0.97	1.12	0.984
GRIMM	98	1.08	-0.26	0.962
SHARP	98	1.07	1.07	0.969

# TEOM-SES and TEOM40

- Can results be transformed and meet ARM requirements ????
- If so:
  - temperature adj.?
  - Julian Day?
  - Other?

# Relationship between Ammonium Nitrate and Mass Difference (Days < 10°C)



## The Black Box (a.k.a The Fudge Factor)

- $$\frac{C}{\left[ \frac{(1 - 0.03(L - R)P / T [12.798 - 18.393e^{(5423((1/273) - (1/T))})} / (P - 6.11e^{(5423((1/273) - (1/T))}))]}{e^{(5423((1/273) - (1/T))})}} \right] e^{(5423((1/273) - (1/T))})} / (P - 6.11e^{(5423((1/273) - (1/T))}))} (1 - (F - 15)/250) ]}$$

- Where:
- C = Initial PM<sub>2.5</sub> concentration
- L = water content in the lab (about 8.7 g/m<sup>3</sup> for Ottawa)
- P = Atmospheric pressure (hPa)
- F = percent filter load (%)
- R = Relative humidity (%)
- T = Temperature (K)

Theory courtesy of Dennis Fudge,  
B.C. Ministry of Environment

# The Amount of Moisture in the Atmosphere

$$PM_{2.5} = C / [(1-0.03(L-W))(1-(F-15)/250)]$$

Where:

C = Initial PM<sub>2.5</sub> concentration

L = water content in the lab (about 8.0 g/m<sup>3</sup>)

F = percent filter load (%)

W = water content in the ambient air (this depends on the temperature, relative humidity and atmospheric pressure)

$$W = (R P/T)[12.798 - 18.393K / (P - 6.11K)](K / (P - 6.11K))$$

Where:

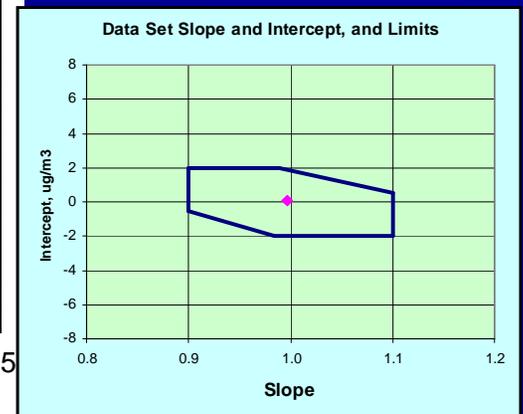
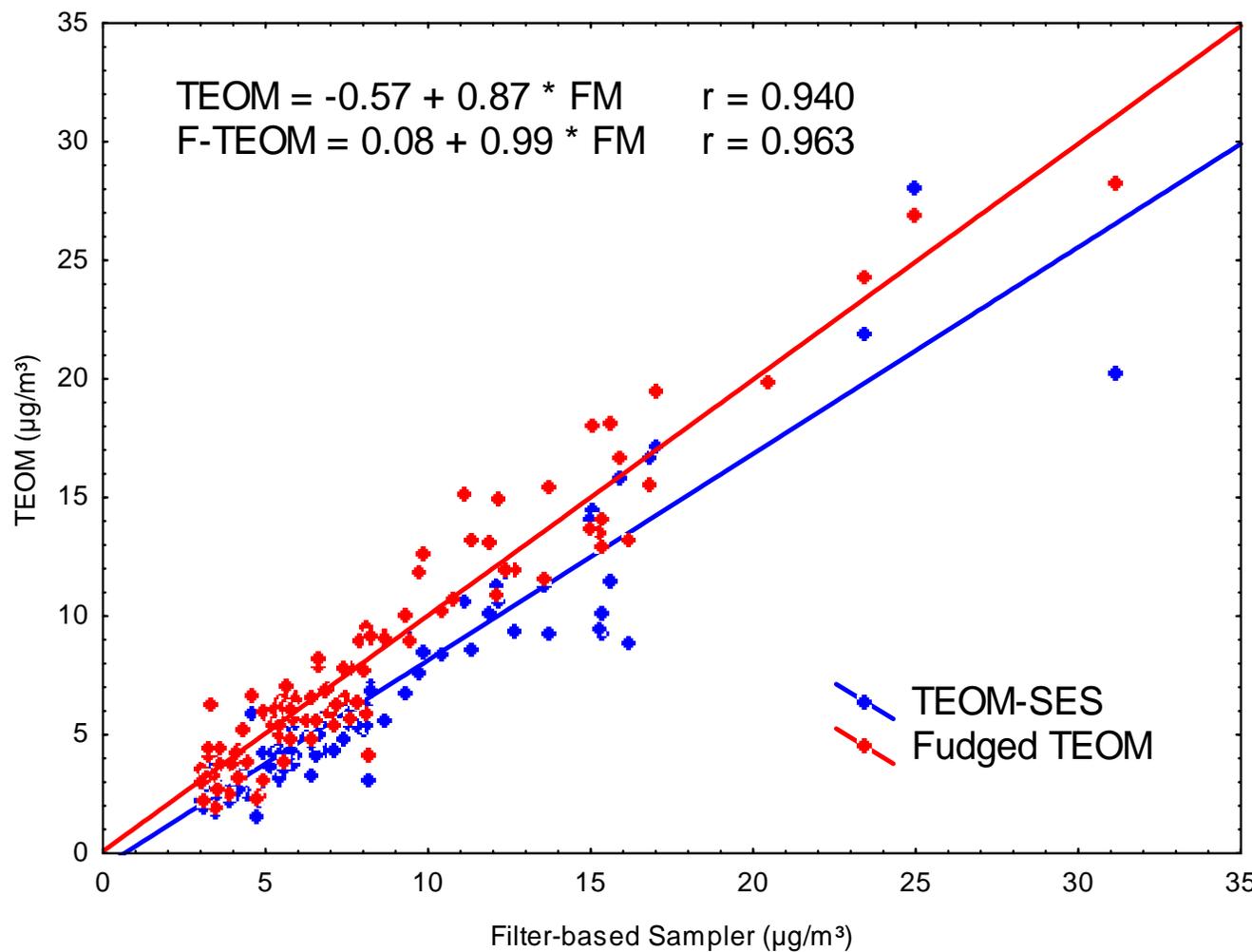
•P = Atmospheric Pressure (hPa)

•T = Temperature (K)

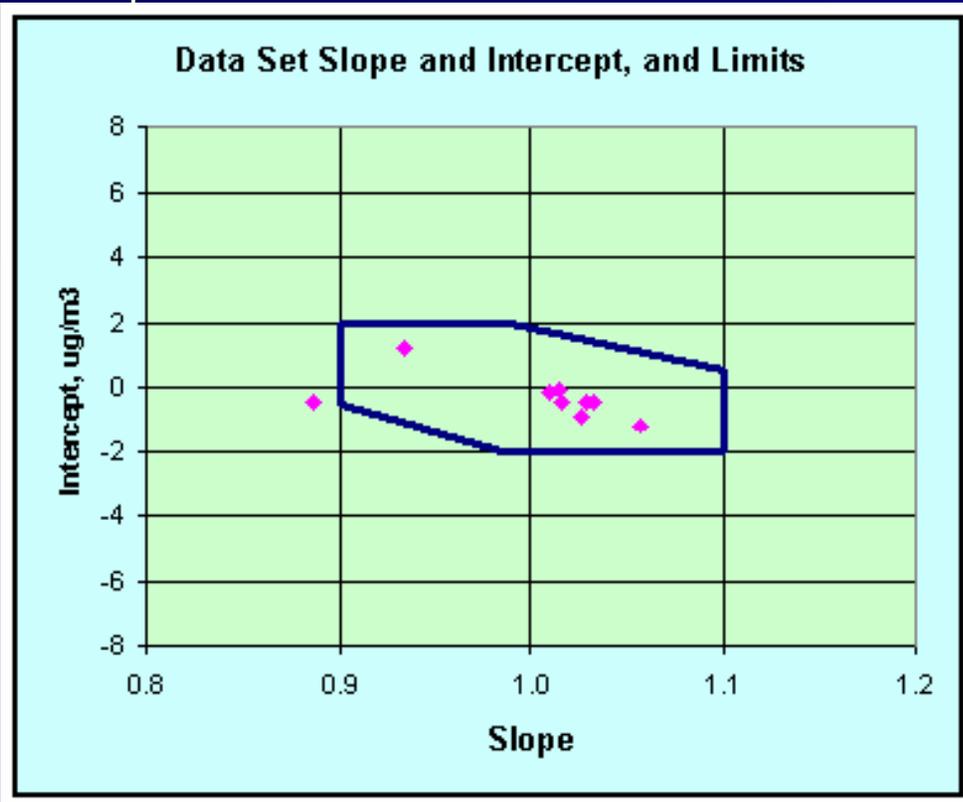
•R = Relative Humidity (%)

•K =  $e^{(5423 * ((1/273) - (1/T)))}$

# Effect on Ottawa TEOM-SES (2007)



# Effect on TEOM40 and TEOM-SES at B.C. Sites (2007)



Site	Correlation (r)
Abbotsford	0.94
Burnaby	0.90
Prince George	0.97
Prince George Plaza	0.98
Vancouver	0.81
Smithers	0.96
Williams Lake	0.96

Theory courtesy of Dennis Fudge,  
B.C. Ministry of Environment